

## ON TWO-DIMENSIONAL DYNAMICAL DISLOCATIONS: THEORETICAL SEISMOGRAMS

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The problem of a two-dimensional dynamical dislocation in an isotropic, homogeneous, unbounded, elastic medium has been discussed by the present authors in a recent paper (SINGH and SIKKA, 1988), assuming harmonic time-dependence. The aim of the present paper is to generalize the results to arbitrary time-dependence. Explicit theoretical expressions for the displacement and the stress components for a two-dimensional dislocation source have been obtained. These expressions can be used to calculate the theoretical seismograms due to a two-dimensional dislocation in an unbounded medium.

### 1. Introduction

The problem of a two-dimensional dynamical dislocation in a uniform unbounded medium has been discussed by several investigators (see, e.g., BOORE *et al.*, 1971; NIAZY, 1973; GELLER, 1974; BOORE and ZOBACK, 1974). In a recent paper (SINGH and SIKKA, 1988; hereinafter referred to as Paper I), we considered in great detail the problem of a two-dimensional dynamical dislocation in infinite and semi-infinite media, assuming harmonic time-dependence. In the present study, we extend the results of Paper I to arbitrary time-dependence of the source.

### 2. Basic Equations

We consider a homogeneous, isotropic, unbounded, elastic medium of density  $\rho$  and elastic parameters  $\lambda, \mu$ . Assuming a harmonic time-dependence  $\exp(-i\omega t)$ , the equations of motion in two-dimensions may be expressed as follows:

$$(\lambda + \mu)\partial_\alpha\partial_\beta u_\beta + \mu\nabla^2 u_\alpha + f_\alpha + \rho\omega^2 u_\alpha = 0, \quad (\text{Plane strain}) \quad (1)$$

$$\mu\nabla^2 u_3 + f_3 + \rho\omega^2 u_3 = 0, \quad (\text{Antiplane strain}) \quad (2)$$

where

$$\partial/\partial x_3 \equiv 0, \quad \partial_i \equiv \partial/\partial x_i, \quad \nabla^2 \equiv \partial_\alpha\partial_\alpha. \quad (3)$$

The summation over repeated suffixes is understood. The Greek subscripts can assume the values 1 and 2 only while the Latin subscripts can assume the values

1, 2, and 3,  $f_i$  is the body force per unit volume, and  $u_i$  are the displacement components.

Let  $G_{\beta}^{\alpha}(Q, P)$  be the  $x_{\alpha}$ -component of the displacement at the point  $Q(x_1, x_2)$  caused by a line force of unit magnitude acting at the point  $P(y_1, y_2)$  in the  $x_{\beta}$ -direction.  $G_{\beta}^{\alpha}(Q, P)$  is similarly defined. Then, displacement field due to a long displacement dislocation can be expressed as line integrals (see Paper I):

Dip-slip

$$u_{\gamma}(Q) = \int_L b \left[ G_{12}^{\gamma} \cos 2\delta + \frac{1}{2} (G_{22}^{\gamma} - G_{11}^{\gamma}) \sin 2\delta \right] ds, \quad (4)$$

Strike-slip

$$u_3(Q) = \int_L b (G_{32}^3 \cos \delta - G_{31}^3 \sin \delta) ds. \quad (5)$$

In Eqs. (4) and (5),  $L$  is the fault section,  $b$  is the magnitude of the dislocation,  $\delta$  is the dip angle and

$$G_{\alpha\beta}^{\gamma}(Q, P) = -\lambda \delta_{\alpha\beta} \partial_{\epsilon} G_{\epsilon}^{\gamma} - \mu (\partial_{\alpha} G_{\beta}^{\gamma} + \partial_{\beta} G_{\alpha}^{\gamma}), \quad (6)$$

$$G_{3\beta}^3(Q, P) = -\mu \partial_{\beta} G_{\beta}^3. \quad (7)$$

For the stress field, we have the following results:

Dip-slip

$$p_{\gamma\epsilon}(Q) = \int_L b \left[ G_{12}^{\gamma\epsilon} \cos 2\delta + \frac{1}{2} (G_{22}^{\gamma\epsilon} - G_{11}^{\gamma\epsilon}) \sin 2\delta \right] ds, \quad (8)$$

Strike-slip

$$p_{3\alpha}(Q) = \int_L b (G_{32}^{3\alpha} \cos \delta - G_{31}^{3\alpha} \sin \delta) ds. \quad (9)$$

In Eqs. (8) and (9),

$$G_{\alpha\beta}^{\gamma\epsilon} = \lambda \delta_{\gamma\epsilon} \partial_{\theta} G_{\alpha\beta}^{\theta} + \mu (\partial_{\gamma} G_{\alpha\beta}^{\epsilon} + \partial_{\epsilon} G_{\alpha\beta}^{\gamma}), \quad (10)$$

$$G_{3\beta}^{3\alpha} = \mu \partial_{\alpha} G_{\beta}^3. \quad (11)$$

Explicit expressions for  $G_{\alpha\beta}^{\gamma}$ , etc., in terms of the Hankel functions of the first kind  $H_m(x) = H_m^{(1)}(x)$  have been obtained in Paper I.

### 3. Theoretical Seismograms

The expressions for the Green's functions  $G_{\alpha}^{\beta}$ ,  $G_{\beta}^3$ ,  $G_{\alpha\beta}^{\gamma}$ ,  $G_{3\beta}^3$ ,  $G_{\alpha\beta}^{\gamma\epsilon}$ , and  $G_{3\beta}^{3\alpha}$  given in Paper I are valid for a harmonic time-dependence,  $\exp(-i\omega t)$ . We next generalize these results to an arbitrary time-dependence. In the following, if  $g(\omega)$  is the harmonic solution, the corresponding time-domain solution is denoted by  $g(t|f)$ , assuming

the time-dependence of the source to be  $f(t)$ . Let

$$g_m(R, c_\alpha; \omega) = \frac{i}{4} e^{m\pi i/2} H_m(K_\alpha R) e^{-i\omega t}, \quad K_\alpha = \omega/c_\alpha. \quad (12)$$

However, we know that (MAGNUS *et al.*, 1966; p. 81)

$$\pi H_m(z) = -2ie^{-m\pi i/2} \int_0^\infty e^{iz \cosh u} \cosh(mu) du. \quad (0 < \arg z < \pi)$$

Therefore, assuming that  $\omega$  is complex with very small imaginary part which is positive, we obtain

$$e^{m\pi i/2} H_m(K_\alpha R) = \frac{2}{\pi i} \int_0^\infty e^{iK_\alpha R \cosh u} \cosh mu du \quad (13)$$

$$= \frac{2}{\pi i} \int_R^\infty \frac{e^{iK_\alpha S}}{(S^2 - R^2)^{1/2}} \cosh[m \cosh^{-1}(S/R)] dS, \quad (14)$$

where  $S = R \cosh u$ . Using the integral representation (14) of the Hankel function of the first kind and order  $m$ , we have

$$g_m(R, c_\alpha; \omega) = \frac{1}{2\pi} \int_R^\infty \frac{e^{-i\omega(t-S/c_\alpha)}}{(S^2 - R^2)^{1/2}} \cosh[m \cosh^{-1}(S/R)] dS. \quad (15)$$

It is now apparent that corresponding to the harmonic solution  $g_m(R, c_\alpha; \omega)$ , the time-domain solution is given by

$$g_m(R, c_\alpha; t|f) = \frac{1}{2\pi} \int_R^\infty \frac{f(t-S/c_\alpha)}{(S^2 - R^2)^{1/2}} \cosh[m \cosh^{-1}(S/R)] dS. \quad (16)$$

Putting  $S/c_\alpha = t'$ , Eq. (16) becomes

$$g_m(R, c_\alpha; t|f) = \frac{1}{2\pi} \int_{R/c_\alpha}^\infty \frac{f(t-t')}{(t'^2 - R^2/c_\alpha^2)^{1/2}} \cosh[m \cosh^{-1}(c_\alpha t'/R)] dt'. \quad (17)$$

Therefore,  $g_m(R, c_\alpha; t|f)$  can be regarded as the convolution of  $f(t)$  with the function

$$\frac{1}{2\pi} H\left(t - \frac{R}{c_\alpha}\right) \frac{\cosh[m \cosh^{-1}(c_\alpha t/R)]}{(t^2 - R^2/c_\alpha^2)^{1/2}}, \quad (18)$$

where  $H(t)$  denotes the Heaviside unit-step function.

If the source acts only for a finite time, so that  $f(t) = 0$  except in the interval  $0 < t < \tau$ , Eq. (17) reveals that, for  $t - \frac{R}{c_\alpha} \gg \tau$ ,

$$g_m(R, c_\alpha; t|f) = \frac{1}{2\pi} H\left(t - \frac{R}{c_\alpha}\right) \frac{\cosh[m \cosh^{-1}(c_\alpha t/R)]}{(t^2 - R^2/c_\alpha^2)^{1/2}} \int_0^\tau f(T) dT. \quad (19)$$

Equation (19) gives the well-known "tail" typical to two-dimensional wave propagation.

If  $f(t)=0$  for  $t<0$ , Eq. (16) should be replaced by

$$g_m(R, c_\alpha; t|f) = \frac{1}{2\pi} H\left(t - \frac{R}{c_\alpha}\right) \int_R^{c_\alpha t} \frac{f(t-S/c_\alpha)}{(S^2 - R^2)^{1/2}} \cosh[m \cosh^{-1}(S/R)] dS. \quad (20)$$

The time-domain expressions for the displacement components for a line force,  $G_\alpha^\beta$  and  $G_3^3$ , the displacement components for a displacement dislocation,  $G_{\alpha\beta}^\gamma$  and  $G_{3\beta}^3$ , and the stress components for a displacement dislocation,  $G_{\alpha\beta}^{\gamma\epsilon}$  and  $G_{3\beta}^{\gamma\epsilon}$  can now be obtained from Eqs. (24)–(29) of Paper I. We find

$$\begin{aligned} G_\alpha^\beta(t|f) = & \frac{1}{2\mu} \left[ \left(\frac{c_2}{c_1}\right)^2 \{ \delta_{\alpha\beta} g_0(R, c_1; t|f) \right. \\ & - (\delta_{\alpha\beta} - 2X_\alpha X_\beta) g_2(R, c_1; t|f) \} \\ & + \delta_{\alpha\beta} g_0(R, c_2; t|f) \\ & \left. + (\delta_{\alpha\beta} - 2X_\alpha X_\beta) g_2(R, c_2; t|f) \right], \quad (21) \end{aligned}$$

$$G_3^3(t|f) = \frac{1}{\mu} g_0(R, c_2; t|f), \quad (22)$$

$$\begin{aligned} G_{\alpha\beta}^\gamma(t|f) = & \frac{1}{2c_2} \left[ \left(\frac{c_2}{c_1}\right)^3 \left\{ \left( 2\frac{2A-1}{1-A} \delta_{\alpha\beta} X_\gamma + \sum \delta_{\beta\gamma} X_\alpha \right) g_1(R, c_1; t|f') \right. \right. \\ & - \left. \left. \left( \sum \delta_{\beta\gamma} X_\alpha - 4X_\alpha X_\beta X_\gamma \right) g_3(R, c_1; t|f') \right\} \right. \\ & + \left. \left( \sum \delta_{\beta\gamma} X_\alpha - 2\delta_{\alpha\beta} X_\gamma \right) g_1(R, c_2; t|f') \right. \\ & \left. + \left( \sum \delta_{\beta\gamma} X_\alpha - 4X_\alpha X_\beta X_\gamma \right) g_3(R, c_2; t|f') \right], \quad (23) \end{aligned}$$

$$G_{3\beta}^3(t|f) = \frac{1}{c_2} X_\beta g_1(R, c_2; t|f'), \quad (24)$$

$$\begin{aligned} G_{\alpha\beta}^{\gamma\epsilon}(t|f) = & \frac{\mu}{6c_2^2} \left[ -3 \left(\frac{c_2}{c_1}\right)^4 \left\{ 2\frac{2A-1}{1-A} \left(\frac{c_1}{c_2}\right)^2 \delta_{\alpha\beta} \delta_{\gamma\epsilon} \right. \right. \\ & + \left. \left. \sum \delta_{\alpha\beta} \delta_{\gamma\epsilon} \right\} g_0(R, c_1; t|f'') \right. \\ & + 4 \left(\frac{c_2}{c_1}\right)^4 \left\{ 3\frac{2A-1}{1-A} (\delta_{\alpha\beta} \delta_{\gamma\epsilon} - \delta_{\alpha\beta} X_\gamma X_\epsilon - \delta_{\gamma\epsilon} X_\alpha X_\beta) \right. \\ & \left. \left. + \sum \delta_{\alpha\beta} \delta_{\gamma\epsilon} - \sum \delta_{\alpha\beta} X_\gamma X_\epsilon \right\} g_2(R, c_1; t|f'') \right. \end{aligned}$$

$$\begin{aligned}
 & -\left(\frac{c_2}{c_1}\right)^4 \left( \sum \delta_{\alpha\beta} \delta_{\gamma\epsilon} - 4 \sum \delta_{\alpha\beta} X_\gamma X_\epsilon + 24 X_\alpha X_\beta X_\gamma X_\epsilon \right) g_4(R, c_1; t | f'') \\
 & - 3 \left( \sum \delta_{\alpha\beta} \delta_{\gamma\epsilon} - 2 \delta_{\alpha\beta} \delta_{\gamma\epsilon} \right) g_0(R, c_2; t | f'') \\
 & + 2 \left( \sum \delta_{\alpha\beta} \delta_{\gamma\epsilon} - 3 \delta_{\alpha\beta} \delta_{\gamma\epsilon} + 3 \delta_{\alpha\beta} X_\gamma X_\epsilon + 3 \delta_{\gamma\epsilon} X_\alpha X_\beta \right. \\
 & \left. - \sum \delta_{\alpha\beta} X_\gamma X_\epsilon \right) g_2(R, c_2; t | f'') \\
 & \left. + \left( \sum \delta_{\alpha\beta} \delta_{\gamma\epsilon} - 4 \sum \delta_{\alpha\beta} X_\gamma X_\epsilon + 24 X_\alpha X_\beta X_\gamma X_\epsilon \right) g_4(R, c_2; t | f'') \right], \quad (25)
 \end{aligned}$$

$$G_{3\beta}^{3\alpha}(t | f) = \frac{\mu}{2c_2^2} \left[ -\delta_{\alpha\beta} g_0(R, c_2; t | f'') + (\delta_{\alpha\beta} - 2X_\alpha X_\beta) g_2(R, c_2; t | f'') \right], \quad (26)$$

where a prime denotes differentiation with respect to the argument. Moreover,

$$\begin{aligned}
 \delta_{\alpha\beta} &= \text{Kronecker delta,} \\
 R^2 &= (x_1 - y_1)^2 + (x_2 - y_2)^2, \\
 X_\alpha &= (x_\alpha - y_\alpha)/R, \\
 c_1, c_2 &= \text{P and S wave-velocities,} \\
 A &= (\lambda + \mu)/(\lambda + 2\mu).
 \end{aligned}$$

The symbols  $\Sigma \delta_{\alpha\beta} \delta_{\gamma\epsilon}$ , etc., are defined in Paper I.

In the derivation of Eqs. (23)–(26), we have made use of the results that the time-domain solution corresponding to  $-i\omega g(R, c_\alpha; \omega)$  is  $g(R, c_\alpha; t | f')$  and the time-domain solution corresponding to

$$-\omega^2 g(R, c_\alpha; \omega) \text{ is } g(R, c_\alpha; t | f'').$$

For vertical dip-slip and vertical strike-slip dislocations, Eqs. (20), (23), and (24) yield the following explicit expressions representing displacements:

$$\begin{aligned}
 G_{12}^1(t | f) &= \frac{1}{4\pi c_2} \left[ \left(\frac{c_2}{c_1}\right)^3 \sin \theta H\left(t - \frac{R}{c_1}\right) \int_R^{c_1 t} \frac{f'(t - S/c_1)}{(S^2 - R^2)^{1/2}} \left(\frac{S}{R}\right) dS \right. \\
 & + \left(\frac{c_2}{c_1}\right)^3 \sin 3\theta H\left(t - \frac{R}{c_1}\right) \int_R^{c_1 t} \frac{f'(t - S/c_1)}{(S^2 - R^2)^{1/2}} \left(4 \frac{S^3}{R^3} - 3 \frac{S}{R}\right) dS \\
 & + \sin \theta H\left(t - \frac{R}{c_2}\right) \int_R^{c_2 t} \frac{f'(t - S/c_2)}{(S^2 - R^2)^{1/2}} \left(\frac{S}{R}\right) dS \\
 & \left. - \sin 3\theta H\left(t - \frac{R}{c_2}\right) \int_R^{c_2 t} \frac{f'(t - S/c_2)}{(S^2 - R^2)^{1/2}} \left(4 \frac{S^3}{R^3} - 3 \frac{S}{R}\right) dS \right], \quad (27 a) \\
 G_{12}^2(t | f) &= \frac{1}{4\pi c_2} \left[ \left(\frac{c_2}{c_1}\right)^3 \cos \theta H\left(t - \frac{R}{c_1}\right) \int_R^{c_1 t} \frac{f'(t - S/c_1)}{(S^2 - R^2)^{1/2}} \left(\frac{S}{R}\right) dS \right.
 \end{aligned}$$

$$\begin{aligned}
& -\left(\frac{c_2}{c_1}\right)^3 \cos 3\theta H\left(t-\frac{R}{c_1}\right) \int_R^{c_1 t} \frac{f'(t-S/c_1)}{(S^2-R^2)^{1/2}} \left(4\frac{S^3}{R^3}-3\frac{S}{R}\right) dS \\
& + \cos \theta H\left(t-\frac{R}{c_2}\right) \int_R^{c_2 t} \frac{f'(t-S/c_2)}{(S^2-R^2)^{1/2}} \left(\frac{S}{R}\right) dS \\
& + \cos 3\theta H\left(t-\frac{R}{c_2}\right) \int_R^{c_2 t} \frac{f'(t-S/c_2)}{(S^2-R^2)^{1/2}} \left(4\frac{S^3}{R^3}-3\frac{S}{R}\right) dS \Big], \quad (27b)
\end{aligned}$$

$$G_{31}^3(t|f) = \frac{1}{2\pi c_2} \cos \theta H\left(t-\frac{R}{c_2}\right) \int_R^{c_2 t} \frac{f'(t-S/c_2)}{(S^2-R^2)^{1/2}} \left(\frac{S}{R}\right) dS, \quad (28)$$

where

$$X_1 = \cos \theta, \quad X_2 = \sin \theta.$$

It can be easily seen that

$$G_0^y = G_{11}^y + G_{22}^y = G_{xx}^y$$

corresponds to the displacement field due to a dilatational line source. From Eqs. (20) and (23), we find

$$\begin{aligned}
G_0^R(t|f) &= G_0^1 \cos \theta + G_0^2 \sin \theta \\
&= \frac{A}{\pi c_1} H\left(t-\frac{R}{c_1}\right) \int_R^{c_1 t} \frac{f'(t-S/c_1)}{(S^2-R^2)^{1/2}} \left(\frac{S}{R}\right) dS, \quad (29) \\
G_0^\theta(t|f) &= G_0^2 \cos \theta - G_0^1 \sin \theta = 0.
\end{aligned}$$

Equation (29) represents P waves with purely radial displacements.

Consider the particular case in which  $f(t) = H(t)$ . Equations (27)–(29) then yield

$$\begin{aligned}
G_{12}^1(t|H) &= \frac{1}{4\pi} \left[ \left(\frac{c_2}{c_1}\right)^2 H\left(t-\frac{R}{c_1}\right) \frac{c_1 t}{R} (c_1^2 t^2 - R^2)^{-1/2} \left\{ \sin \theta + \left(4\frac{c_1^2 t^2}{R^2} - 3\right) \sin 3\theta \right\} \right. \\
& \left. + H\left(t-\frac{R}{c_2}\right) \frac{c_2 t}{R} (c_2^2 t^2 - R^2)^{-1/2} \left\{ \sin \theta - \left(4\frac{c_2^2 t^2}{R^2} - 3\right) \sin 3\theta \right\} \right], \quad (30a)
\end{aligned}$$

$$\begin{aligned}
G_{12}^2(t|H) &= \frac{1}{4\pi} \left[ \left(\frac{c_2}{c_1}\right)^2 H\left(t-\frac{R}{c_1}\right) \frac{c_1 t}{R} (c_1^2 t^2 - R^2)^{-1/2} \left\{ \cos \theta - \left(4\frac{c_1^2 t^2}{R^2} - 3\right) \cos 3\theta \right\} \right. \\
& \left. + H\left(t-\frac{R}{c_2}\right) \frac{c_2 t}{R} (c_2^2 t^2 - R^2)^{-1/2} \left\{ \cos \theta + \left(4\frac{c_2^2 t^2}{R^2} - 3\right) \cos 3\theta \right\} \right], \quad (30b)
\end{aligned}$$

$$G_{31}^3(t|H) = \frac{1}{2\pi} H\left(t-\frac{R}{c_2}\right) \frac{c_2 t}{R} (c_2^2 t^2 - R^2)^{-1/2} \cos \theta, \quad (31)$$

$$G_0^R(t|H) = \frac{A}{\pi} H\left(t-\frac{R}{c_1}\right) \frac{c_1 t}{R} (c_1^2 t^2 - R^2)^{-1/2}, \quad (32)$$

where we have used the relations

$$H'(t - S/c_a) = \delta(t - S/c_a) = c_a \delta(S - c_a t).$$

Taking the limit as  $t \rightarrow \infty$ , Eqs. (30)–(32) give

$$G_{12}^1 = \frac{1}{4\pi R} [(2 - A) \sin \theta + A \sin 3\theta], \quad (33)$$

$$G_{12}^2 = \frac{1}{4\pi R} [(2 - A) \cos \theta - A \cos 3\theta], \quad (34)$$

$$G_{31}^3 = \frac{1}{2\pi R} \cos \theta, \quad G_0^R = \frac{A}{\pi R}. \quad (35)$$

Equations (33)–(35) coincide with the corresponding statical results.

The displacement  $G_{31}^3(t|H)$  in Eq. (31) falls from  $\infty$  at  $t = R/c_2$  and approaches the static limit  $(1/2\pi R) \cos \theta$  at  $t \rightarrow \infty$ . Writing

$$t = \frac{R}{c_a} + \tau_a \quad (\tau_a > 0), \quad (36)$$

we get, for small values of  $s_2 = c_2 \tau_2 / R$ ,

$$G_{31}^3(t|H) \sim \frac{\cos \theta}{2\pi R} H(\tau_2) \left[ \frac{1}{\sqrt{2s_2}} \left( 1 + \frac{3}{4} s_2 \right) \right]. \quad (37)$$

The displacement consists of a sudden jerk at  $t = R/c_2$ , followed by a gradual recovery, which is incomplete.

For small values of  $s_1 = c_1 \tau_1 / R$ , Eq. (30 a) yields, for the P pulse,

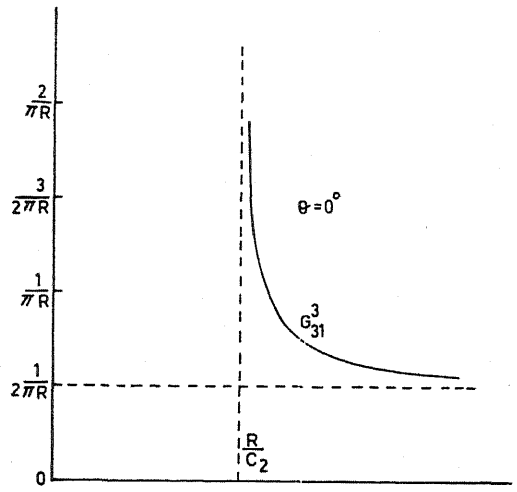
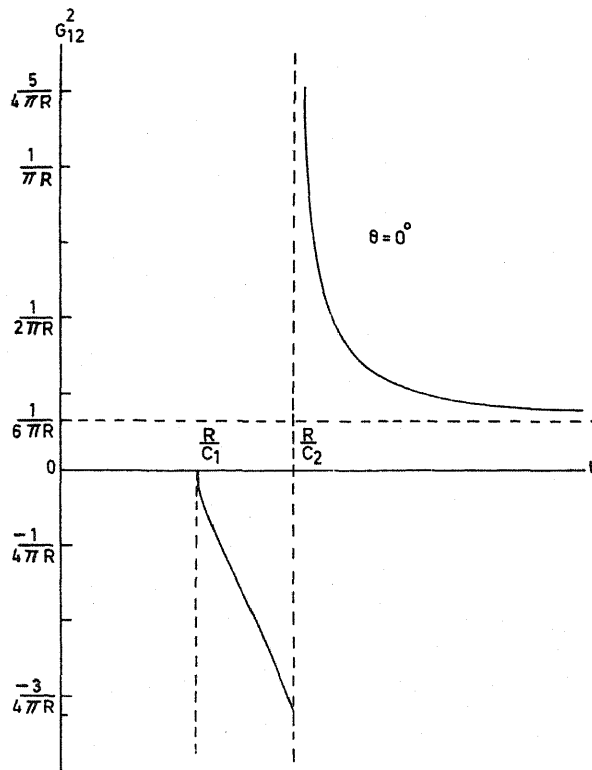
$$G_{12}^1(t|H) \sim \frac{1 - A}{4\pi R} H(\tau_1) \left[ \frac{1}{\sqrt{2s_1}} \left( 1 + \frac{3}{4} s_1 \right) \sin \theta + \frac{1}{\sqrt{2s_1}} \left( 1 + \frac{35}{4} s_1 \right) \sin 3\theta \right]. \quad (38)$$

Similarly, for small values of  $s_2 = c_2 \tau_2 / R$ , we find, for the S pulse,

$$G_{12}^1(t|H) \sim \frac{1}{4\pi R} H(\tau_2) \left[ \frac{1}{\sqrt{2s_2}} \left( 1 + \frac{3}{4} s_2 \right) \sin \theta - \frac{1}{\sqrt{2s_2}} \left( 1 + \frac{35}{4} s_2 \right) \sin 3\theta \right]. \quad (39)$$

In this case, the displacement consists of a sudden jerk at  $t = R/c_1$  (P pulse), another sudden jerk at  $t = R/c_2$  (S pulse), followed by a gradual recovery, which is incomplete.

Figure 1 shows the variation of  $G_{31}^3$  with  $t$  for  $\theta = 0^\circ$ . Figures 2, 3, and 4 show the variation of  $G_{12}^2$  with  $t$  for  $\theta = 0^\circ, 30^\circ$ , and  $60^\circ$ , respectively, for the Poisson case  $c_1 = \sqrt{3} c_2$ . When  $\theta = 0^\circ$ ,  $G_{12}^2$  increases from 0 to  $-\sqrt{6}/3\pi R$  as  $t$  increases

Fig. 1. Variation of  $G_{31}^3$  with  $t$  for  $\theta = 0^\circ$ .Fig. 2. Variation of  $G_{12}^2$  with  $t$  for  $\theta = 0^\circ$ .



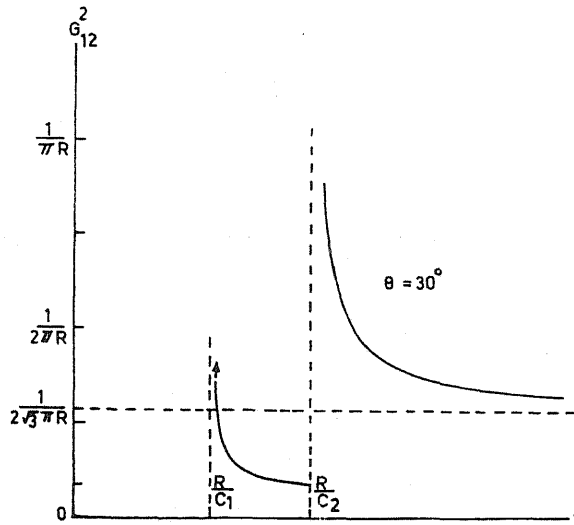


Fig. 3. Variation of  $G_{12}^2$  with  $t$  for  $\theta = 30^\circ$ .

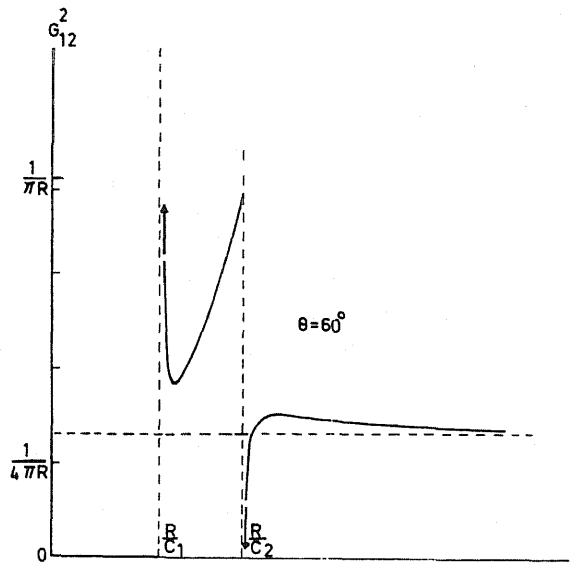


Fig. 4. Variation of  $G_{12}^2$  with  $t$  for  $\theta = 60^\circ$ .

from  $R/c_1$  to  $R/c_2$ . There is a sudden jerk at  $R/c_2$  followed by a gradual recovery to the static limit  $1/6\pi R$ . For  $\theta = 30^\circ$ , there is a sudden jerk at  $R/c_1$  followed by another jerk at  $R/c_2$ . For  $\theta = 60^\circ$ ,  $G_{12}^2 \rightarrow -\infty$  as  $t \rightarrow R/c_2 + 0$ . Thus, we notice that the behaviour of  $G_{12}^2$  strongly depends upon the angle  $\theta$ . The variation of  $G_{12}^2$  is

similar to the variation of  $G_{12}^2$ . The following relations follow from Eqs. (30 a) and (30 b).

$$G_{12}^1(\theta = 30^\circ) = G_{12}^2(\theta = 60^\circ),$$

$$G_{12}^1(\theta = 60^\circ) = G_{12}^2(\theta = 30^\circ),$$

$$G_{12}^1(\theta = 90^\circ) = G_{12}^2(\theta = 0^\circ).$$

Neglecting  $1/R^{3/2}$  and higher powers of  $1/R$ , we have the following far-field approximations obtained from Eqs. (30 a, b):

$$G_{12}^1(t|H) = \frac{(1-A)H(\tau_1)}{2\pi(2c_1\tau_1R)^{1/2}} \cos \theta \sin 2\theta - \frac{H(\tau_2)}{2\pi(2c_2\tau_2R)^{1/2}} \sin \theta \cos 2\theta, \quad (40)$$

$$G_{12}^2(t|H) = \frac{(1-A)H(\tau_1)}{2\pi(2c_1\tau_1R)^{1/2}} \sin \theta \sin 2\theta + \frac{H(\tau_2)}{2\pi(2c_2\tau_2R)^{1/2}} \cos \theta \cos 2\theta. \quad (41)$$

Therefore,

$$G_{12}(t|H) = e_1 G_{12}^1(t|H) + e_2 G_{12}^2(t|H) = \frac{(1-A)H(\tau_1)}{2\pi(2c_1\tau_1R)^{1/2}} \sin 2\theta e_R + \frac{H(\tau_2)}{2\pi(2c_2\tau_2R)^{1/2}} \cos 2\theta e_\theta.$$

The first term in Eq. (42) corresponds to P waves and the second term corresponds to S waves. The far-field displacements decay with distance as  $R^{-1/2}$ . Moreover, the ratio of the far-field S wave amplitude to the far-field P wave amplitude is about  $(c_1/c_2)^{5/2}$ , which is roughly equal to 4, if  $\lambda = \mu$ .

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