

AN APPLICATION OF THE THEORY OF FINITE STRAIN

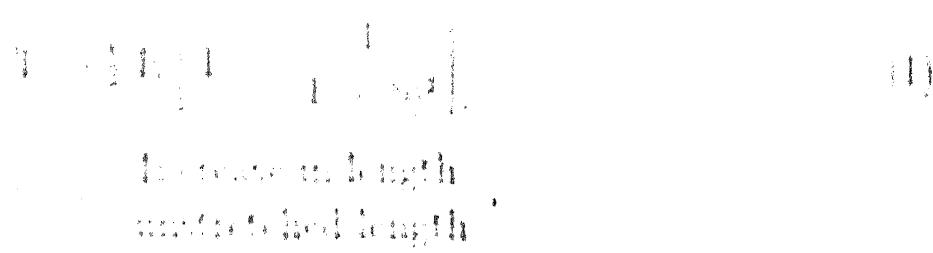
John D. Cook

Department of Mechanical Engineering

University of Michigan

The theory of finite strain has been developed in the literature by a number of authors, and it is now well known that the theory of finite strain is capable of predicting the behavior of materials under large strains. However, the theory of finite strain is not yet fully developed, and there are still many problems which remain to be solved. One of the most important problems is the prediction of the behavior of materials under large strains. This problem is particularly important because the behavior of materials under large strains is often quite different from their behavior under small strains. For example, when a material is subjected to a large strain, it may exhibit a significant change in its mechanical properties, such as its yield strength, its modulus of elasticity, and its ductility. These changes are often quite different from those observed under small strains.

In this paper, we will consider a simple model of a beam under a large strain. We will assume that the beam is made of a linear elastic material, and that the strain is uniformly distributed along the length of the beam. We will also assume that the beam is initially straight, and that the strain is small, but not when compared to the yield strain. Under these conditions, the generalized Hooke's Law can be used to predict the behavior of the beam under large strains. The generalized Hooke's Law states that the stress and strain are connected by means of



the equation $\sigma = E \epsilon$, where σ is the stress, E is the modulus of elasticity, and ϵ is the strain.

If x is measured downwards from the fixed point, the equation of motion is

$$\frac{m d^2x}{dt^2} = mg - \frac{1}{2} E \left(1 - \frac{l^2}{x^2} \right). \quad (2)$$

Putting $y = x/l$, we have on integration

$$\frac{1}{2} ml \left(\frac{dy}{dt} \right)^2 = (mg - \frac{1}{2} E) y - \frac{1}{2} \frac{E}{y} + C, \quad (3)$$

C being a constant of integration.

Now the velocity of the particle vanishes at two points in its line of motion. Let these be given by $y = \alpha$ and $y = \beta$ ($\alpha > \beta$). We can rewrite (3) as

$$\frac{1}{2} ml \left(\frac{dy}{dt} \right)^2 = (\frac{1}{2} E - mg) \frac{(\alpha - y)(y - \beta)}{y}, \quad (4)$$

where

$$\alpha \beta = \frac{E}{E - 2mg}. \quad (5)$$

$T = mg = \frac{1}{2} E$ gives infinite elongation, and hence corresponds to the yield point. Therefore, $mg < \frac{1}{2} E$.

From (4) we see that t and y are connected by means of the elliptic integral of the second kind, viz.,

$$t = \sqrt{\frac{ml}{E - 2mg}} \int_y^\alpha \frac{y dy}{\sqrt{y(\alpha - y)(y - \beta)}} \quad (6)$$

Putting $y = \alpha(1 - k^2 \sin^2 \phi)$, where $k^2 \alpha = (\alpha - \beta)$, we get

$$\begin{aligned} t &= 2 \sqrt{\alpha} \cdot \sqrt{\frac{ml}{E - 2mg}} \int_0^\phi \sqrt{1 - k^2 \sin^2 \phi} d\phi \\ &= 2 \sqrt{\alpha} \cdot \sqrt{\frac{ml}{E - 2mg}} E(k, \phi). \end{aligned} \quad (7)$$

But

$$mg = \frac{1}{2} E \left[1 - \frac{1}{(1 + L/l)^2} \right],$$

or

$$\sqrt{\frac{E}{E - 2mg}} = 1 + \frac{L}{l}, \quad (8.1)$$

so that

$$\alpha \beta = \left(1 + \frac{L}{l} \right)^2. \quad (8.2)$$

Putting

$$k^2 = 1 - \frac{\beta}{\alpha} = \sin^2 \theta,$$

we get,

$$\alpha = \left(1 + \frac{L}{l} \right) \sec \theta = \frac{l'}{l} \sec \theta, \quad (8.3)$$

and Amplitude = $l(\alpha - \beta) = l\left(1 + \frac{L}{l}\right)\sin\theta\tan\theta$
 $= l'\sin\theta\tan\theta,$ (8.4)

where l' is the stretched length in the position of equilibrium.

We can now rewrite (7) as

$$t = 2\sqrt{\frac{ml}{E}} \left(\frac{l'}{l}\right)^{\frac{3}{2}} \sqrt{\sec\theta} E(k, \phi). \quad (9)$$

The period of a complete oscillation is, therefore, given by

$$T = 4\sqrt{\frac{ml}{E}} \left(\frac{l'}{l}\right)^{\frac{3}{2}} \sqrt{\sec\theta} E_0, \quad (10)$$

E_0 being the complete elliptic integral of the second kind.

If Hooke's Law is adopted, the period is known to be

$$T_0 = 2\pi\sqrt{\frac{ml}{E}}. \quad (11)$$

Hence,

$$\frac{T}{T_0} = \frac{2}{\pi} E_0 \left(\frac{l'}{l}\right)^{\frac{3}{2}} \sqrt{\sec\theta}. \quad (12)$$

As the amplitude increases with both θ and l' , the ratio (T/T_0) increases with the amplitude.

The variation of $(2/\pi) E_0 \sqrt{\sec\theta}$ and $\sin\theta\tan\theta$ with respect to θ is given in the following table :

TABLE

| θ | 0° | 10° | 20° | 30° | 40° | 50° | 60° | 70° | 80° | 90° |
|---------------------------------|-----------|------------|------------|------------|------------|------------|------------|------------|------------|------------|
| $(2/\pi) E_0 \sqrt{\sec\theta}$ | 1 | 1.000 | 1.001 | 1.004 | 1.014 | 1.037 | 1.090 | 1.217 | 1.589 | ∞ |
| $\sin\theta\tan\theta$ | 0 | 0.031 | 0.124 | 0.289 | 0.539 | 0.913 | 1.500 | 2.582 | 5.585 | ∞ |

It is clear from the table that the period does not vary very much with the amplitude for small values of θ . But this variation cannot be neglected when θ exceeds 40° .

For a given value of θ we see from (12) that

$$(T/T_0)^2 \propto l'^3,$$

which shews that the variation of (T/T_0) with l' follows the law of the semi-cubical parabola.