

# Boundary element method based computation of stress intensity factor by modified crack closure integral

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**Abstract** The local smoothing scheme in conjunction with the modified crack closure integral technique has been adopted in the boundary element method to improve the accuracy of computed stress intensity factors. Simple relations have been derived for the case of linear, quadratic and quarter point elements around the crack tip. Case studies are presented to demonstrate improvement in the accuracy. While the displacement method gives a difference with the standard handbook solution up to 26%, the suggested method helps to reduce it to within 2%.

## List of symbols

$G_I, G_{II}$	strain energy release rate in mode I, mode II
$K$	stress intensity factor
$l$	crack tip element length
$P$	total load
$p_1, p_2$	tractions
$r_1, r_2$	internal and external radii
$s_{avg}, s_j$	x-component of traction
$t, t_1, t_2, t_{avg}, t_j$	y-component of traction
$u$	x-component of displacement
$v$	y-component of displacement
$W$	crack closure work
$x, y$	cartesian coordinates
$Y$	SIF correction factor
$\xi$	natural coordinate

## 1

### Introduction

The boundary element method (BEM) provides an attractive alternative to finite element method (FEM) for the extraction of stress intensity factors (SIFs). The issue has received a considerable attention, e.g. Cruse and Buren (1971), Cruse (1972, 1978), Cruse and Wilson (1978), Tan and Fenner (1978, 1979), Nadiri et al. (1982), Bakr and

Fenner (1985), Perucchio and Ingraffea (1985) and Gerstle (1988). The SIFs can be evaluated in principle using several methods, e.g. displacement and stress method (Watwood 1969, Chan et al. 1970), weight function technique, J-integral method (Rice 1968), stiffness derivative procedure (Parks 1974), crack closure integral (Irwin 1958), etc., for 2-D crack configurations. Out of these the first two has been mostly adopted in the BEM.

In the BEM displacements and tractions are used as independent variables. This offers scope for imposing different rates of variation for the two entities. While using the analog of the wellknown quarter point finite element (Barsoum 1976) in the BEM, the assumption of a variation of displacement in proportion to square root of distance from the crack tip does guarantee a square root strain singularity. This cannot however automatically ensure a square-root traction singularity. Blandford et al. (1981) and Martinez et al. (1984) have shown that more accurate SIFs are obtained employing the traction singularity elements than strain singularity elements. They have employed the displacement based extrapolation method for the extraction of the SIFs.

In the FEM, the adoption of the concept of modified crack closure integral (CCI) have contributed to the improvement of accuracy of SIFs over the computation based on the displacement method. This has been demonstrated by several investigators, e.g. Rybicki and Kanninen (1977), Krishnamurthy et al. (1985), Ramamurthy et al. (1986) and Sethuraman and Maiti (1988). The method can also help obtaining solution for problems with mixed mode loading. This technique was first adopted in the FEM by Rybicki and Kanninen (1977) to evaluate the SIF. They explained the method considering a linear variation of the displacement field around the crack tip. Consequently, the element ensures a constant strain field. They termed the method as modified crack closure integral technique. Later it has been shown by Krishnamurthy et al. (1985), Ramamurthy et al. (1986) and Sethuraman and Maiti (1988) that crack line displacement and stresses can be locally smoothed using the computed nodal data. These smoothed field can then be employed to compute the crack closure work. This procedure gives the energy release rate, and hence the SIFs, which are more accurate than the results based on displacement method or the modified CCI. The similar possibility has not yet been exploited in the BEM. This has provided the motivation for the present study. The formulation is presented and the performance is illustrated for the case of linear, quadratic and quarter point elements used around the crack tips.

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## 2.1

## Linear element

For a typical BEM discretisation (Fig. 1a), with crack tip at node  $j$  and the two adjacent nodes  $j-1$  and  $j+1$ , the displacement variation over OA can be written in the form

$$v = a_0 + a_1(1 - x/l) \quad (1)$$

where  $a_0$  and  $a_1$  are arbitrary constants,  $l$  is the length of the crack tip element and  $x$  is the coordinate. It is straightforward to show that  $a_0 = 0$  and  $a_1 = v_{j-1}$ . A linear variation of the traction along OB can be represented in the same way as the displacement. That is

$$t = 0.5(t_j + t_{j+1}) - 0.5(t_j - t_{j+1})\xi \quad (2)$$

where  $\xi$  is a natural coordinate. The total load  $P$  on the face OB

$$P = \int_0^l t \, dx = 0.5(t_j + t_{j+1})l \quad (3)$$

In the smoothing scheme the traction variation is assumed consistent with the displacement variation. For a linear element, the traction variation is assumed constant over each element span. The normal traction  $p_1$  over OB is so chosen that the total load  $p_1l = P$ . This gives

$$p_1 = 0.5(t_j + t_{j+1}) \quad (4)$$

In the boundary element formulation the work done corresponding to the span AO of the boundary is not zero, though this segment is free of any normal traction. This is because traction at the node  $j$  is nonzero. The constant traction  $p_2$  along the face AO is assumed to be equal to the

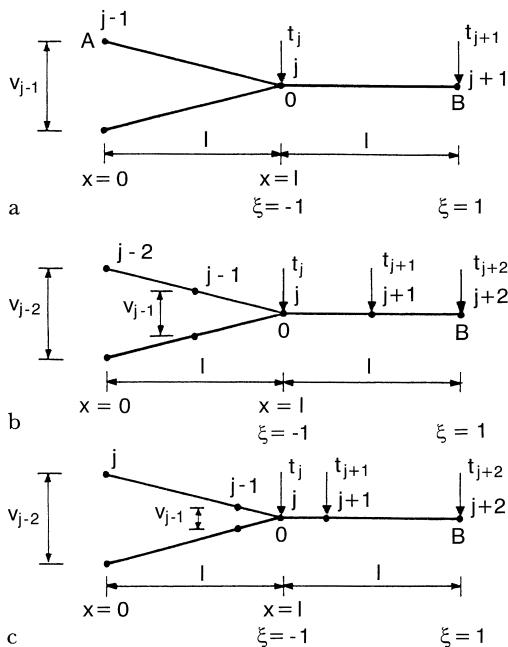


Fig. 1a-c. (a) Linear element. (b) Quadratic element. (c) Quarter point element

traction at the node  $j$  for the crack closure work calculations, i.e.  $p_2 = t_j$ . The total crack closure work  $W$  is given by

$$W = \frac{1}{2} \int_0^l (v p_1 + v p_2) \, dx \quad (5)$$

Finally this leads to

$$G_I = \frac{v_{j-1}}{2} [0.75 t_j + 0.25 t_{j+1}] \quad (6)$$

A similar expression can be derived for mode II, which will involve  $x$  components of tractions and displacements. The SIF can then be obtained using the standard relations between  $G$  and  $K$ .

If the traction  $p_1$  over OB is arbitrarily assumed to be a constant and is equal to  $t_j$ , a different expression for  $G$  is obtained.

$$G_I = v_{j-1} t_j / 2 \quad (7)$$

## 2.2 Quadratic element

In the case of quadratic elements around the crack tip (Fig. 1b) the displacement variation over OB is given by

$$v = v_{j-2} - 0.5 v_{j-1} \xi + (0.5 v_{j-2} - v_{j-1}) \xi^2 \quad (8)$$

Similarly the traction variation, which is also quadratic, has the form

$$t = t_{j+2} + 0.5(t_{j+2} - t_j) \xi + [0.5 (t_{j+2} + t_j) - t_{j+1}] \xi^2 \quad (9)$$

The total normal load arising out of the traction on the face OB

$$P = \int_0^l t \, dx = (t_j + 4t_{j+1} + t_{j+2})l/6 \quad (10)$$

The traction variation for smoothing is assumed to be linear. The variation of traction  $p_1$  along AO is given by

$$p_1 = \frac{1}{2}(1 + \xi) t_j \quad (11)$$

The variation of traction  $p_2$  along OB is assumed to be

$$p_2 = \frac{1}{2}(1 - \xi) t_1 + \frac{1}{2}(1 + \xi) t_2 \quad (12)$$

where  $t_1$  and  $t_2$  are the assumed tractions at the nodes  $j$  and  $j+2$ .  $t_1$  and  $t_2$  are assumed so that the total load is the same as  $P$ .  $t_1$  and  $t_2$  can be taken in the following form

$$t_1 = (t_j + 2 t_{j+1})/3 \quad (13)$$

$$t_2 = (2 t_{j+1} + t_{j+2})/3 \quad (14)$$

The total crack closure work

$$W = \frac{1}{2} \int_0^l (v p_1 + v p_2) \, dx \\ = [2 t_j v_{j-1} + t_1(2 v_{j-1} + v_{j-2}) + 2 t_2 v_{j-1}] / 12 \quad (15)$$

The strain energy release rate

$$G_I = \frac{1}{6} [t_j v_{j-1} + t_1 (v_{j-1} + 0.5 v_{j-2}) + t_2 v_{j-1}] \quad (16)$$

A similar expression for  $G_{II}$  can be obtained involving x-component of tractions and displacements.

### 2.3

#### Quarter point element

In the case of quarter point elements (Fig. 1c) the displacement is assumed to vary as  $\sqrt{x}$  along OA. That is

$$v = 2(v_{j-2} - 2v_{j-1}) (1 - x/l) + (4v_{j-1} - v_{j-2}) \sqrt{(1 - x/l)} \quad (17)$$

The traction too has a similar variation and can be represented in the form

$$t = t_j \{-0.5 \xi(1 - \xi)\} + t_{j+1}(1 - \xi^2) + t_{j+2}\{0.5 \xi(1 + \xi)\} \quad (18)$$

where  $1 + \xi = 2\sqrt{(x/l)}$ .

The total load over OB

$$P = \int_0^l t \, dx = (2t_{j+1} + t_{j+2})l/3 \quad (19)$$

This equation shows that the total load is independent of the traction at the crack tip node j. Therefore, total load for the span AO is zero, because  $t_{j-1}$  and  $t_{j-2}$  are both zero. Hence the traction  $p_1$  along AO can be neglected. In order to ensure a singularity variation of traction along the span OB and the same total load P, the traction  $p_2$  along OB is taken as follows.

$$p_2 = \frac{t_{avg}}{2\sqrt{(x/l)}} \quad (20)$$

where  $t_{avg} = (2t_{j+1} + t_{j+2})/3$

The total crack closure work

$$W = \frac{1}{2} \int_0^l v p_2 \, dx = 0.5 t_{avg} [v_{j-2} (4/3 - \pi/4) + v_{j-1} (\pi - 8/3)] \quad (22)$$

The strain energy release rate

$$G_I = 0.5 t_{avg} [v_{j-2} (4/3 - \pi/4) + v_{j-1} (\pi - 8/3)] \quad (23)$$

A similar expression can be derived for  $G_{II}$ , the mode II energy release rate.

$$G_{II} = 0.5 s_{avg} [u_{j-2} (4/3 - \pi/4) + u_{j-1} (\pi - 8/3)] \quad (24)$$

where  $s_{avg} = (2s_{j+1} + s_{j+2})/3$ ,  $s_{j+1}$  and  $s_{j+2}$  are the x-components of nodal tractions.

### 3

#### Case studies

Numerical studies have been carried out on mode I considering problems of centre crack, single edge crack and circular ring with radial cracks (Fig. 2). The a/w ratio is considered in the range 0.2 to 0.8 for the centre crack problem (Fig. 2a) and 0.2 to 0.7 for the edge crack problem (Fig. 2b). A similar parameter  $a/(r_2 - r_1)$ , is considered in the range of 0.2 to 0.8 for the circular ring with radial inner edge crack under external uniform tension (Fig. 2c) and 0.1 to 0.6 for the circular ring with radial outer edge crack under internal pressure (Fig. 2d). The material is assumed to be isotropic. In the case of quadratic and quarter point elements the crack tip element size is 0.01a. For the case of linear element the size is 0.005a. The subsequent element sizes, away from the crack tip, are 0.02a, 0.04a, 0.08a, 0.15a, etc. In the case of centre and edge cracks, there are approximately 22 elements and 44 nodes in the discretisation when quadratic and quarter point elements are used around the crack tip. When the linear element is used, the number of elements and nodes are 48. These extra nodes come up because two closely spaced nodes are used at the four corners. In the case of circular ring the number of elements and nodes are 26 and 52 when quadratic and quarter point elements are used. The SIF has been computed through both the displacement and the proposed CCI methods. In the displacement technique the SIF is evaluated considering separately the displacement of the first and second corner nodes from the crack tip. The results in the form of SIF correction factor Y in the case of centre crack, edge crack and radial inner edge crack are compared with the handbook solutions (Rooke and Cartwright, 1976 and Murakami 1987) in Tables 1 to 10 and the data for the case of radial outer edge crack are presented in Table 11.

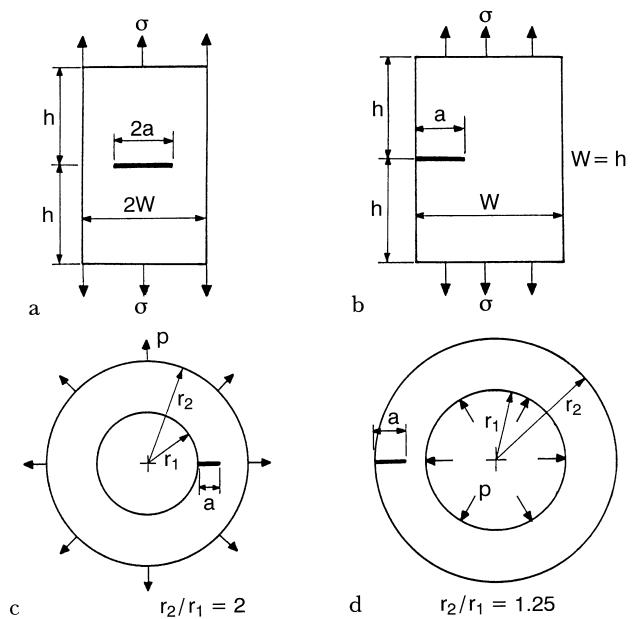


Fig. 2a-d. Geometries considered for analysis. (a) Centre crack. (b) Edge crack. (c) Circular ring with radial inner edge crack. (d) Circular ring with radial outer edge crack

The effect of the crack tip element size on the accuracy of the results has been studied for both the centre crack and edge crack problems considering  $a/w = 0.5$ . The results are shown in Figs. 3 and 4.

#### 4

#### Discussion

The accuracy of the displacement method is dependent on where the displacements are compared. The accuracy improves substantially in the case of linear elements considering the second corner node rather than the first corner node for a comparison. Thereby the maximum error reduces from 27% to about 6.5%. The CCI method

helps to keep this difference to within 11.39% for the centre crack problem. In the case of both quadratic and quarter point elements, the comparison of displacements at the second corner node is preferable. However in these cases, the CCI method gives the best accuracy. The error is less than about 1.5%.

In the case of edge crack in the rectangular panel, again comparison of displacement at the second corner node is preferable. The error is around 30% when linear element is employed and SIF is compared at the first corner node. This error reduces to within 14% for quarter point element and less than 4.2% for quadratic element. The error is within 6% for all the three elements when the SIF is

**Table 1.** Comparison of SIF correction factor Y for centre crack for linear element

a/w	SIF Correction Factor Y						
	Reference Solution	Computed by				CCI Method	
		Displacement Method		1st Corner Node		2nd Corner Node	
		Y	% Error	Y	% Error	Y Eqn. (6)	%Error
0.2	1.0254	0.7611	-25.778	0.9696	-5.443	0.9228	-10.002
0.3	1.0594	0.7831	-26.081	0.9973	-5.862	0.9495	-10.372
0.4	1.1118	0.8205	-26.197	1.0454	-5.972	0.9949	-10.510
0.5	1.1891	0.8760	-26.331	1.1157	-6.174	1.0622	-10.670
0.6	1.3043	0.9988	-23.422	1.2189	-6.547	1.1856	-9.103
0.7	1.4842	1.0859	-26.835	1.4201	-4.317	1.3191	-11.125
0.8	1.7989	1.3121	-27.059	1.7136	-4.745	1.5940	-11.388

**Table 2.** Comparison of SIF correction factor Y for centre crack for quadratic element

a/w	SIF Correction Factor Y						
	Reference Solution	Computed by				CCI Method	
		Displacement Method		1st Corner Node		2nd Corner Node	
		Y	% Error	Y	% Error	Y Eqn. (16)	% Error
0.2	1.0254	0.9743	-4.984	0.9858	-3.864	1.0226	-0.270
0.3	1.0594	1.0079	-4.866	1.0265	-3.110	1.0572	-0.204
0.4	1.1118	1.0567	-4.952	1.0695	-3.808	1.1094	-0.217
0.5	1.1891	1.1293	-5.025	1.1425	-3.918	1.1857	-0.289
0.6	1.3043	1.2332	-5.449	1.2471	-4.385	1.2944	-0.760
0.7	1.4842	1.4020	-5.535	1.4268	-3.868	1.4713	-0.871
0.8	1.7989	1.6938	-5.845	1.7222	-4.265	1.7778	-1.173

**Table 3.** Comparison of SIF correction factor Y for centre crack for quarter point element

a/w	SIF Correction Factor Y						
	Reference Solution	Computed by				CCI Method	
		Displacement Method		1st Corner Node		2nd Corner Node	
		Y	% Error	Y	% Error	Y Eqn. (23)	% Error
0.2	1.0254	1.1384	11.024	1.0343	0.871	1.0157	-0.944
0.3	1.0594	1.1771	11.124	1.0508	-0.816	1.0516	-0.735
0.4	1.1118	1.2352	11.096	1.1220	0.913	1.1023	-0.857
0.5	1.1891	1.3203	11.031	1.1997	0.889	1.1784	-0.898
0.6	1.3043	1.4437	10.686	1.3117	0.571	1.2886	-1.201
0.7	1.4842	1.6398	10.484	1.4626	-1.454	1.4655	-1.263
0.8	1.7989	1.9830	10.236	1.7609	-2.112	1.7727	-1.458

**Table 4.** Comparison for SIF correction factor Y for edge crack for linear element

a/w	SIF Correction Factor Y						
	Reference Solution	Computed by					
		Displacement Method				CCI Method	
		1st Corner Node		2nd Corner Node		Y Eqn. (6)	% Error
		Y	% Error	Y	% Error		
0.2	1.3736	1.0293	-25.066	1.3159	-4.203	1.2471	- 9.207
0.3	1.6629	1.2452	-25.117	1.5951	-4.078	1.5081	- 9.309
0.4	2.1066	1.5763	-25.176	2.0237	-3.933	1.9072	- 9.463
0.5	2.8297	2.0886	-26.191	2.6962	-4.718	2.5257	-10.743
0.6	4.0299	2.9119	-27.743	3.7953	-5.823	3.5141	-12.675
0.7	6.3610	4.4314	-30.335	5.9779	-6.022	5.3575	-15.776

**Table 5.** Comparison for SIF correction factor Y for edge crack for quadratic element

a/w	SIF Correction Factor Y						
	Reference Solution	Computed by					
		Displacement Method				CCI Method	
		1st Corner Node		2nd Corner Node		Y Eqn. (16)	% Error
		Y	% Error	Y	% Error		
0.2	1.3736	1.3160	-4.195	1.3360	-2.738	1.3793	0.418
0.3	1.6629	1.6008	-3.737	1.6272	-2.149	1.6767	0.828
0.4	2.1066	2.0380	-3.257	2.0762	-1.441	2.1315	1.180
0.5	2.8297	2.7284	-3.579	2.7907	-1.379	2.8475	0.627
0.6	4.0299	3.8950	-3.348	4.0091	-0.516	4.0518	0.543
0.7	6.3610	6.1061	-4.007	6.4362	1.182	6.3594	-0.026

**Table 6.** Comparison for SIF correction factor Y for edge crack for quarter point element

a/w	SIF Correction Factor Y						
	Reference Solution	Computed by					
		Displacement Method				CCI Method	
		1st Corner Node		2nd Corner Node		Y Eqn. (23)	% Error
		Y	% Error	Y	% Error		
0.2	1.3736	1.5410	12.186	1.4042	2.230	1.3726	-0.075
0.3	1.6629	1.8755	12.756	1.7117	2.936	1.6695	0.396
0.4	2.1066	2.3903	13.466	2.1870	3.819	2.1245	0.848
0.5	2.8297	3.2052	13.270	2.9441	4.041	2.8433	0.482
0.6	4.0299	4.5911	13.927	4.2438	5.309	4.0582	0.703
0.7	6.3610	7.1817	12.901	6.6361	4.325	6.3669	0.093

**Table 7.** Comparison of SIF correction factor Y for circular ring with radial inner edge crack under external tension for linear element

a/(r <sub>2</sub> -r <sub>1</sub> )	SIF Correction Factor Y						
	Reference Solution	Computed by					
		Displacement Method				CCI Method	
		1st Corner Node		2nd Corner Node		Y Eqn. (6)	% Error
		Y	% Error	Y	% Error		
0.2	2.7760	2.0871	-24.817	2.6256	-5.418	2.5273	- 8.958
0.3	2.8672	2.1237	-25.931	2.6711	-6.841	2.5719	-10.301
0.4	2.9887	2.1948	-26.565	2.7601	-7.646	2.6581	-11.602
0.5	3.1360	2.2679	-27.683	2.8547	-8.970	2.7457	-12.445
0.6	3.3152	2.3919	-27.851	3.0123	-9.137	2.8954	-12.662
0.7	3.5541	2.5502	-28.247	3.2152	-9.535	3.0859	-13.174
0.8	3.9125	2.8202	-27.918	3.5608	-8.989	3.4118	-12.796

**Table 8.** Comparison of SIF correction factor Y for circular ring with radial inner edge crack under external tension for quadratic element

a/(r <sub>2</sub> - r <sub>1</sub> )		SIF Correction Factor Y					
Reference Solution	Computed by	Displacement Method				CCI Method	
		1st Corner Node		2nd Corner Node		Y Eqn. (16)	% Error
		Y	% Error	Y	% Error		
0.2	2.7760	2.6380	-4.972	2.6624	-4.094	2.7620	-0.503
	2.8672	2.7193	-5.160	2.7441	-4.293	2.8476	-0.682
	2.9887	2.8386	-5.022	2.8648	-4.146	2.9726	-0.539
	3.1360	2.9663	-5.413	2.9955	-4.479	3.1041	-1.017
	3.3152	3.1395	-5.301	3.1721	-4.315	3.2837	-0.950
	3.5541	3.3513	-5.705	3.3889	-4.648	3.5019	-1.468
	3.9125	3.6982	-5.478	3.7434	-4.322	3.8604	-1.331

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**Table 9.** Comparison of SIF correction factor Y for circular ring with radial inner edge crack under external tension for quarter point element

a/(r <sub>2</sub> - r <sub>1</sub> )		SIF Correction Factor Y					
Reference Solution	Computed by	Displacement Method				CCI Method	
		1st Corner Node		2nd Corner Node		Y Eqn. (23)	% Error
		Y	% Error	Y	% Error		
0.2	2.7760	3.0793	10.927	2.8635	3.153	2.7394	-1.301
	2.8672	3.1768	10.800	2.9537	3.018	2.8274	-1.388
	2.9887	3.3191	11.054	3.0862	3.261	2.9540	-1.160
	3.1360	3.4685	10.603	3.2273	2.913	3.0849	-1.629
	3.3152	3.6739	10.818	3.4201	3.163	3.2657	-1.493
	3.5541	3.9247	10.428	3.6567	2.888	3.4856	-1.929
	3.9125	4.3384	10.888	4.0462	3.416	3.8489	-1.625

**Table 10.** Comparison of SIF correction factor Y based on a different scheme of CCI calculation for centre crack, edge crack and circular ring with radial inner edge crack for linear element

a/w	SIF Correction Factor Y Computed by Eqn. (7)					
	Centre crack		Edge crack		Circular ring	
	Y	% Error	Y	% Error	Y	% Error
0.2	1.1016	-1.348	1.3673	-0.460	2.7713	-0.170
0.3	1.0408	-1.753	1.6535	-0.563	2.8200	-1.647
0.4	1.0906	-1.906	2.0914	-0.719	2.9145	-2.484
0.5	1.1644	-2.081	2.7703	-2.099	3.0108	-3.993
0.6	1.2721	-2.470	3.8597	-4.224	3.1751	-4.227
0.7	1.4440	-2.711	5.8736	-7.662	3.3842	-4.7781
0.8	1.7449	-3.000	-	-	3.7421	-4.355

compared at the second corner node. The CCI method helps to contain the error within 16% in the case of linear element. The error reduces drastically when the quadratic or quarter point elements are employed around the crack tip. The maximum error is 1.18% for the range of  $a/w = 0.2$  to  $0.7$  for both the quadratic and quarter point elements. Similar trend is observed in the case of circular rings. The error is found to be less than 2% for the range of  $a/(r_2 - r_1) = 0.2$  to  $0.8$  when quadratic or quarter point elements are employed in the proposed method.

The error in Y through Eqn. (6) is in the range of 10–16% in the case of centre crack, edge crack and circular

ring with inner edge crack. However, if Eqn. (7) is employed instead (Table 10), the error reduces to within 3% in the case of centre crack, 7.66% for the edge crack and 4.8% for the circular ring. This means that an assumption of a constant traction  $p_1 = t_j$  over the edge OB produces better results than the assumption of a value  $p_1 = (t_j + t_{j+1})/2$ . It is not possible to provide any justification for this observation at this stage.

The results for the case of circular ring with radial outer edge crack (Table 11) shows that, for  $a/w$ , for example, equal to 0.3, the difference with Rooke and Cartwright (1976) is less than 10%, 1.62% and 1% based on linear

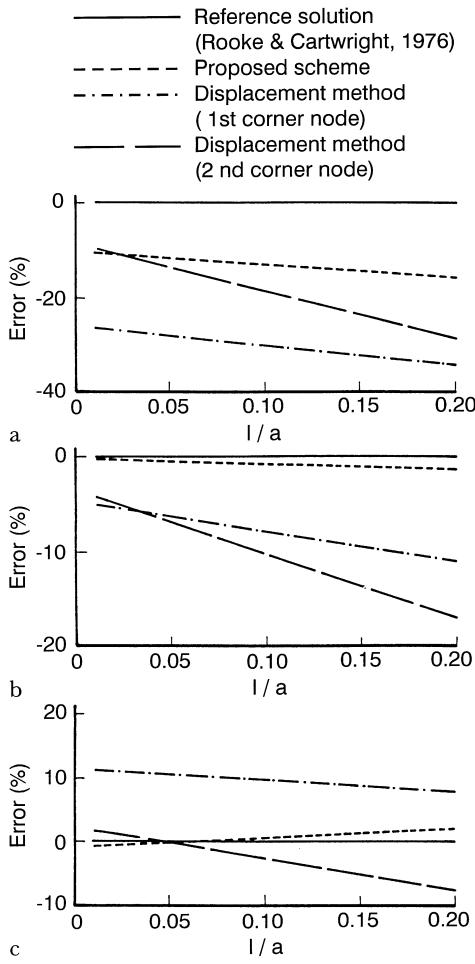


Fig. 3a-c. Effect of crack tip element size on error in the case of centre crack. (a) Linear element. (b) Quadratic element. (c) Quarter point element

element, quadratic element and quarter point element respectively with adoption of the CCI.

The effect of crack tip element size on the accuracy of SIF shows (Figs. 3 and 4) that the displacement method is very sensitive to the crack tip element size. The accuracy reduces as the element size increases. On the other hand the proposed method is less sensitive to the mesh refinement. In the case of the linear elements the difference with the reference solution increases steadily with the element size. The minimum difference observed is about 10% for a crack tip element size of 0.01a for both the cases. In the

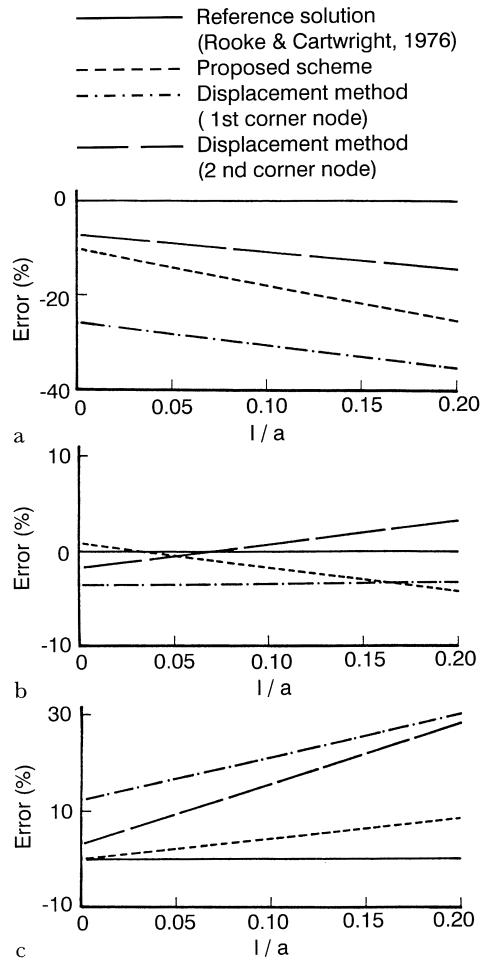


Fig. 4a-c. Effect of crack tip element size on error in the case of edge crack. (a) Linear element. (b) Quadratic element. (c) Quarter point element

case of quadratic elements, for a crack tip element size up to 0.2a, the difference is around 1% for the centre crack and it is less than 4.5% for the edge crack. In the case of the quarter point elements there is very good accuracy for element size up to 0.12a in the case of centre crack problem and 0.06a in the case of edge crack.

## 5 Conclusion

Thus it is clear that the crack closure integral and local smoothing can be used together to improve the accuracy

Table 11. SIF correction factor Y for circular ring with radial outer edge crack using CCI method

a/(r <sub>2</sub> -r <sub>1</sub> )	SIF Correction Factor Y Computed By		
	Linear element		Quadratic element
	Y	Y	Y
0.1	1.085	1.1649	1.1619
0.2	1.2012	1.3088	1.3008
0.3	1.3860	1.5650	1.5551
0.4	1.6557	1.8296	1.8213
0.5	2.0271	2.2416	2.2337
0.6	2.4653	2.7271	2.7174

of boundary element based computation of SIFs. While locally smoothing the traction and displacement variation along the crack line, it is beneficial to keep the order of displacement variation the same as in the BEM but the order of traction variation one order less than the displacement. By adopting the CCI along with local smoothing the error can be reduced to less than 1% in the case of mode I problems. In general the crack tip element size less than about  $0.06a$  is recommended.

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