

Available online at www.sciencedirect.com



Applied Catalysis A: General 308 (2006) 128-133



www.elsevier.com/locate/apcata

Direct oxidation of H_2 to H_2O_2 over Pd-based catalysts: Influence of oxidation state, support and metal additives

V.R. Choudhary^a, C. Samanta^a, T.V. Choudhary^{b,*}

^a Chemical Engineering Division, National Chemical Laboratory, Pune 411008, India ^b 5518 Colony Court, Bartlesville, OK 74006, USA

Received 23 November 2005; received in revised form 3 April 2006; accepted 15 April 2006 Available online 23 May 2006

Abstract

The influence of oxidation state (reduced and oxidized), support (ZrO₂, Ga₂O₃, CeO₂, SiO₂, H- β , ThO₂, CeO₂–ZrO₂, BPO₄ and Pd/Al₂O₃) and precious metal additives (Au, Pt, Rh and Ru) on the direct H₂O₂ synthesis has been investigated over Pd-based catalysts. For all the supports investigated herein, the oxidized Pd catalysts showed significantly superior H₂O₂ yields as compared to their reduced counterparts. The effect of the Pd oxidation state was found to be more important for determining the H₂O₂ yields than the particle size and surface area properties of the catalysts system. An excellent correlation was observed between the H₂O₂ selectivity and H₂O₂ decomposition activity of the oxidized Pd catalysts. The oxidized Pd catalysts showed almost an order of magnitude lower H₂O₂ decomposition activity than the reduced catalysts. The H₂O₂ yield in the H₂ to H₂O₂ oxidation passed through a maximum with increase in the Au concentration. Although a similar effect was also observed in case of Pt, Au was found to be a superior promoter for the direct H₂O₂ synthesis process. Addition of Rh and Ru was found to be detrimental for the H₂O₂ yields; these results can be explained in terms of increased H₂O₂ decomposition activity and/or enhanced H₂ to H₂O reaction activity in their presence. © 2006 Elsevier B.V. All rights reserved.

Keywords: H₂O₂; Direct synthesis; Decomposition; Pd catalysts; Metal additives; Oxidation state; Supports

1. Introduction

 H_2O_2 , which is an environmentally benign oxidant, is expected to play an increasingly important role in the chemical industry [1]. Other applications of H_2O_2 (such as bleach in the textile and pulp/paper industry and in treatment of waste water) are also on the rise, thus indicating the need for larger volumes of H_2O_2 . The current commercial process for H_2O_2 production is a circuitous process involving indirect oxidation of H_2 (Anthraquinone process). Since the above process is quite complex, there is a significant interest in developing a direct H_2 oxidation process [2]. Direct synthesis of H_2O_2 has received considerable attention [1–14] in recent years with Pd-based systems as the catalysts of choice. In the H_2 to H_2O_2 oxidation over the Pd catalysts, the selective H_2O_2 ($H_2 + O_2 \rightarrow H_2O_2$) and non-selective water ($H_2 + 0.5O_2 \rightarrow H_2O$) forming reactions occur simultaneously. Furthermore, the H_2O_2 molecules are unstable in presence of Pd which further facilitates its conversion to water. It is, therefore, extremely difficult to achieve high H_2O_2 selectivity/yields. Since the side reaction involving combustion of hydrogen to water is a highly exothermic reaction, increasing the H_2O_2 selectivity is also important for making the process non-hazardous. The challenges posed by the direct H_2O_2 process, therefore, make it an interesting candidate for study from a scientific as well as a commercial viewpoint.

Our previous studies have suggested that oxidation state of Pd also plays a role in determining the activity/selectivity in the direct H_2 oxidation to H_2O_2 process [6]. Herein, we have systematically considered this aspect by investigating the effect of Pd oxidation state on the H_2O_2 yields over several supported Pd catalysts (Pd/ZrO₂, Pd/Ga₂O₃, Pd/CeO₂, Pd/SiO₂ and Pd/H- β , Pd/ThO₂, Pd/CeO₂–ZrO₂, Pd/BPO₄ and Pd/Al₂O₃). H_2O_2 decomposition studies have also been undertaken on these catalysts (Pd in reduced and unreduced state) to gain further insights into the process.

Hutchings and coworkers observed that Au-based catalysts exhibited high H_2O_2 selectivity, but low H_2O_2 formation rates

^{*} Corresponding author. *E-mail address:* tvchoud@yahoo.com (T.V. Choudhary).

⁰⁹²⁶⁻⁸⁶⁰X/\$ - see front matter © 2006 Elsevier B.V. All rights reserved. doi:10.1016/j.apcata.2006.04.010

at low reaction temperatures (2 °C) in a solvent mixture of methanol and water [8]. However, a considerable increase in H_2O_2 formation rate was observed when Au was coupled with Pd in the catalyst system. It is therefore interesting to study the influence of different metal additives (and their content) on the direct H_2O_2 synthesis. Herein, we have investigated the H_2O_2 synthesis and decomposition at 25 °C in an acidic medium over the following precious metal added Pd-based systems:

- (a) Pd-Au/ZrO₂ (Au/Pd atom ratio range = 0-0.11)
- (b) Pd-Pt (Pt/Pd atom ratio range = 0-0.09)
- (c) Pd-Rh (Rh/Pd atom ratio range = 0-0.16)
- (d) Pd-Ru (Ru/Pd atom ratio range = 0-0.16)

2. Experimental

2.1. Catalyst synthesis

2.1.1. Supported Pd catalysts

The Al₂O₃ (prepared from bohemite by its calcination at 500 °C for 2 h), ZrO₂ (prepared from zirconyl nitrate by its hydrolysis to zirconium hydroxide by ammonium hydroxide and calcining at 500 °C for 2 h), Ga₂O₃, CeO₂, ThO₂ (prepared from thorium nitrate by its hydrolysis to thorium hydroxide by ammonium hydroxide and calcining at 500 °C for 2 h), SiO₂ (prepared from B-type silica gel, by calcining at 500 °C for 3 h), CeO₂-ZrO₂ (prepared by mixing CeO₂ and ZrO₂ with Ce/ Zr mole ratio of 1.0, in the presence of deionised water just sufficient to form a thick paste, drying the wet mixture in an air oven at 100 °C for 2 h and then calcining it in air at 600 °C for 3 h), H- β (Si/Al = 27 and crystal size = 1.0 μ m) and BPO₄ (prepared from a mixture of boric acid and orthophosphoric acid with B/P mole ratio of 1.0, drying the mixture in air oven at 100 °C for 2 h and then calcining it in air at 600 °C for 3 h) supported oxidized Pd (2.5 wt%) catalysts were prepared by impregnating the respective support with palladium acetate from its acetonitrile solution by the incipient wet impregnation technique. After impregnation, the wet catalyst mass was dried at 100 °C for 2 h and then calcined under static air in a muffle furnace at 500 °C for 3 h.

The supported reduced Pd catalyst was prepared from the respective oxidized Pd catalyst by reducing it with an ammoniacal hydrazine solution at room temperature (27 $^{\circ}$ C) for 2 h followed by washing, filtration and drying at 100 $^{\circ}$ C in an air oven.

2.1.2. Bimetallic catalysts

The ZrO₂ supported bimetallic catalysts (e.g. Au-Pd/ZrO₂, Pt-Pd/ZrO₂, Ru-Pd/ZrO₂ and Rh-Pd/ZrO₂) with different noble metal (Au, Pt, Ru and Rh) loadings and constant Pd loading (2.5 wt%) were prepared by simultaneously impregnating fine particles of ZrO₂ with the corresponding noble metal chlorides from their aqueous acidic solution by the incipient wetness technique, drying at 100 °C for 2 h and then calcining in static air at 500 °C for 3 h.

2.2. Catalyst characterization

The Pd⁰ and/or PdO phases in the supported Pd catalysts were determined by X-ray powder diffraction method using a Holland Phillips, PW/1730 X-ray generator with Cu K α radiation ($\lambda = 1.5406$ Å; 40 kV, 25 Ma). The surface area of the catalysts was measured by the single point BET method by measuring the adsorption of nitrogen at liquid N₂ temperature and at the N₂ concentration of 30 mol% (balance helium), using a Monosorb Surface Area Analyzer (Quantachrome Corp., USA) based on dynamic adsorption/desoption technique. Before carrying out surface area measurement experiments, the catalyst (0.1–1.0 g) was pretreated in situ in the sample cell at 300 °C for 1 h in flow of (30 cm³ min⁻¹) of a mixture of helium and nitrogen to remove the traces of moisture.

2.3. Reaction procedure

2.3.1. H_2O_2 synthesis

The direct oxidation of H₂ by O₂ to H₂O₂ over the supported Pd catalysts was carried out at atmospheric pressure (95 kPa) in a magnetically stirred glass reactor (capacity 250 cm^3) containing 0.5 g catalyst in a fine power form and an aqueous acidic solution (150 cm³) as a reaction medium. A H_2/O_2 $(4.6 \text{ mol}\% \text{ H}_2)$ gas mixture was bubbled (using a fine glass tip) continuously through the reaction medium containing the catalyst under vigorous stirring at a constant temperature. The temperature of the reaction was controlled by continuously passing water through the reactor jacket from thermostatic bath. The concentration of unreacted hydrogen present in the effluent gases, after removing the water vapors from them by condensation at 0 °C, was measured by an online hydrogen analyzer (Kathorometer, Nucon, New Delhi) based on a thermal conductivity detector. After the reaction, the solid catalyst from the reaction mixture was separated by filtration and the filtrate was analyzed for the H₂O₂ formed in the reaction by iodometric titration. The conversion of H2, H2O2 yield and selectivity were obtained as follows:

$$H_2$$
 conversion (%)
(moles of H_2 in the feed)

$$= \frac{-(\text{moles of } H_2 \text{ in the effluent gases})}{\text{moles of } H_2 \text{ in the feed}} \times 100$$

$$H_2O_2 \text{ yield } (\%) = \frac{\text{moles of } H_2O_2 \text{ formed}}{\text{moles of } H_2 \text{ in the feed}} \times 100$$

$$H_2O_2 \text{ selectivity } (\%) = \frac{\text{moles of } H_2O_2 \text{ formed}}{\text{moles of } H_2 \text{ consumed}} \times 100$$

Some of the experiments were repeated and an excellent reproducibility ($\pm 5\%$ for H₂O₂ yields) was observed for these experiments. The repeatability of the iodometric titration experiments in terms of determining H₂O₂ concentration was within 3%. Constant calibrations were undertaken to ensure the accuracy of the analysis. The flammability and detonability limits for H₂ in O₂ (at 25 °C and 1 atm pressure) are 4.0% H₂ (lower) to 94% H₂ (upper) and 15% H₂ (lower) to 90% H₂

(upper), respectively. The process could be hazardous when operated within the flammability limits, particularly when the flammable reaction mixture is ignited or subjected to a dry Pd catalyst. The safety in the present work was ensured by using the feed H_2/O_2 mixture close to the lower flammability limit, so that the concentration of H_2 in the reactor exit gas was less than 4.0% and also care was taken to avoid spillage of catalyst on the reactor walls during the reaction. The H_2 gas flow rate was very small (0.7 ml/min); however, a flame arrester for H_2 (a 100 cm long and 3.0 mm o.d. ss tube packed with glass beads) was used between the H_2 cylinder and reactor to avoid flame propagation back to the H_2 cylinder, as a precautionary measure.

2.3.2. H_2O_2 decomposition

The H_2O_2 decomposition reaction over the catalysts was carried out using a magnetically stirred glass reactor (capacity: 250 cm³) containing 0.2 g catalyst in 150 cm³ aqueous reaction medium, with or without containing acid and/or halide anions, by injecting 1 ml of 30% (w/v) H_2O_2 solution in the reactor under vigorous stirring and measuring the gas (O₂) evolved in the H_2O_2 decomposition at 25 °C and atmospheric pressure, as a function of time, using a constant pressure gas collector [15]. The percent H_2O_2 decomposition data was estimated as follows:

H₂O₂ decomposition (%) =
$$\frac{V_t}{V_T} \times 100$$

where V_t is the volume of O_2 evolved in time t and V_T is the volume of O_2 evolved in the complete decomposition of H_2O_2 in the reactor. The H_2O_2 decomposition activity of the supported Pd catalysts was evaluated in term of a first order rate constant (k) according to the first order rate expression: $\ln [V_T/(V_T - V_t)] = kC_A t$ (where V_T is the volume of O_2 evolved in the complete H_2O_2 decomposition, V_t the volume of O_2 evolved in time t and C_A is the catalyst concentration/loading).

3. Results and discussions

3.1. Effect of mass transfer on the reaction between H_2 and O_2

The rate of the reaction between the H_2 and O_2 in liquid medium is known to depend on the mass transfer of the reactants to the catalyst sites [8]. It is, therefore, important that experiments to investigate the formation of H_2O_2 in the reaction between H_2 and O_2 should be carried out under conditions at which the mass transfer has minimal influence on the reaction rate. Fig. 1 shows the conversion of H_2 for different agitation rates with all other variables remaining constant. The stirring speed was adjusted by altering the applied voltage (V) to the magnetic stirrer. At the lower stirring speeds, the conversion of H_2 was found to depend



Fig. 1. Effect of the stirring speed on the conversion of H_2 in the reaction between H_2 and O_2 over the reduced Pd/C catalyst in aqueous acidic (0.03 M H_3PO_4) reaction medium [reaction conditions: volume of the reaction medium = 150 cm³, amount of catalyst = 0.5 g, H_2 concentration in O_2 = 4.6 mol%, reaction temperature = 25 °C and reaction period = 3 h].



Fig. 2. Results of the direct oxidation of H_2 to H_2O_2 over different reduced Pd catalysts (Pd loading = 2.5 wt%) [reaction conditions: reaction medium = 0.03 M H_3PO_4 , volume of reaction medium = 150 cm³, amount of catalyst = 0.5 g, reaction temperature = 25 °C, H_2 concentration in O_2 = 4.6 mol% and reaction period = 3 h].



Fig. 3. Results of the direct oxidation of H_2 to H_2O_2 over different oxidized Pd catalysts (Pd loading = 2.5 wt%) [reaction conditions: reaction medium = 0.03 M H_3PO_4 , volume of reaction medium = 150 cm³, amount of catalyst = 0.5 g, reaction temperature = 25 °C, H_2 concentration in O_2 = 4.6 mol% and reaction period = 3 h].

on the stirring speed. However, above 230 V there was no significant change in the H_2 conversion, indicating the absence of gas–liquid mass transfer effect on the reaction. For the subsequent experiments, the stirrer speed was fixed at 260 V.

3.2. Influence of the Pd oxidation state on the H_2 to H_2O_2 reaction over different supported Pd catalysts

Figs. 2 and 3 reveal the performance of the different supported Pd catalysts in the H₂ to H₂O₂ oxidation with Pd in the reduced (Pd⁰) and oxidized state (PdO), respectively. The H₂O₂ decomposition activity for the different catalysts is also

shown. The H₂ conversion activity of the reduced catalysts was higher than that for the oxidized forms. However, the oxidized Pd catalysts had a considerably higher selectivity for the H₂O₂ formation. Also, the H₂O₂ decomposition activity was an order of magnitude higher for the reduced Pd catalysts. The higher H₂O₂ decomposition activity for the reduced Pd catalysts may be related to the higher propensity for H₂O₂ adsorption on reduced Pd sites.

In case of the direct H_2 oxidation process, the selectivity for H_2O_2 may decrease either due to combustion side reaction $(H_2 + 0.5O_2 \rightarrow H_2O)$ or secondary reactions of H_2O_2 leading to further water formation. Therefore, a lowering of the H_2O_2



Fig. 4. Variation of H_2O_2 selectivity (SH₂O₂) in the H_2 to H_2O_2 oxidation with the H_2O_2 decomposition activity for the different supported oxidized (a) and reduced (b) Pd catalysts (k_d = pseudo-first order H_2O_2 decomposition rate constant).

 Table 1

 Surface and bulk properties of the different reduced Pd catalysts

Catalyst	Surface area $(m^2 g^{-1})$	Average Pd particle size (nm)
Pd (2.5%)/Al ₂ O ₃	176.0	24.0 ^a
Pd (2.5%)/Ga ₂ O ₃	36.0	22.0^{a}
Pd (2.5%)/CeO ₂	18.0	45.0 ^b
Pd (2.5%)/ZrO ₂	59.0	54.0 ^b
Pd (2.5%)/ThO ₂	1.0	-
Pd (2.5%)/SiO ₂	231.0	12.0 ^a
Pd (2.5%)/CeO ₂ -ZrO ₂	8.0	-
Pd (2.5%)/BPO ₄	25.0	-
Pd (2.5%)/H-β	165.0	18.0 ^a

^a Determined by using Scherrer's formula.

^b Obtained from TEM.

conversion activity of the catalyst should increase the H_2O_2 selectivity in the H_2 to H_2O_2 oxidation. In line with this, a good correlation was observed between the selectivity for H_2O_2 in the H_2 to H_2O_2 oxidation process and the H_2O_2 decomposition activity for the oxidized catalysts (Fig. 4a). Metal particle size and surface area data for the different reduced Pd catalysts are shown in Table 1. The properties of the reduced Pd catalysts were found to be less important in determining the H_2O_2 yield/ selectivity in the H_2 to H_2O_2 oxidation. The reduced Pd catalysts in general, gave more or less similar results (little or no H_2O_2 selectivity) in the H_2 to H_2O_2 oxidation because of their extremely high H_2O_2 decomposition activity (Fig. 2).

3.3. Effect of metal additives

Results showing the influence of gold (Au) concentration in the oxidized Pd-Au/ZrO₂ catalyst on its performance in the H₂ to H₂O₂ oxidation reaction at 25 °C in an aqueous acidic (0.03 M



Fig. 5. Influence of the concentration of gold loading in the oxidized Pd/ZrO₂ catalyst on the: (a) H₂ to H₂O₂ oxidation and (b) H₂O₂ decomposition rate constant (k_d) in aqueous acidic (0.03 M H₃PO₄) reaction medium (at 25 °C).



Fig. 6. Influence of the concentration of Pt in the oxidized Pd $(2.5\%)/ZrO_2$ catalyst on the: (a) H₂ to H₂O₂ oxidation and (b) H₂O₂ decomposition rate constant (k_d) in aqueous acidic (0.03 M H₃PO₄) reaction medium (at 25 °C).

 H_3PO_4) medium are presented in Fig. 5a. The H_2 conversion over the catalyst was found to increase with the increasing gold loading in the catalyst. However, the H_2O_2 yield in the H_2 to H_2O_2 oxidation initially increased (more than doubled) and then decreased slightly with increase in the Au concentration. Thus, an optimum Au concentration is required for achieving high H_2O_2 yields in the reaction under the investigated experimental



Fig. 7. Influence of the concentration of Ru in the oxidized Pd $(2.5\%)/ZrO_2$ catalyst on the: (a) H₂ to H₂O₂ oxidation and (b) H₂O₂ decomposition rate constant (k_d) in aqueous acidic (0.03 M H₃PO₄) reaction medium (at 25 °C).



Fig. 8. Influence of the concentration of Rh in the oxidized Pd (2.5%)/ZrO₂ catalyst on the: (a) H₂ to H₂O₂ oxidation and (b) H₂O₂ decomposition rate constant (k_d) in aqueous acidic (0.03 M H₃PO₄) reaction medium (at 25 °C).

conditions. The observed lower H_2O_2 yield at the higher Au concentration in the catalyst may be attributed to the higher H_2O_2 decomposition activity of the catalyst, as shown in Fig. 5b. The initial increase in H_2O_2 yield may be related to the decrease in the H_2 to H_2O side reaction (due to presence of Au). Previous studies have shown that Au catalysts show a high selectivity for H_2O_2 formation in the direct H_2O_2 synthesis process [8]. This may be related to the ability of the Au to form stable hydroperoxy species which are considered to be the precursors for H_2O_2 [16]. The increase in the secondary decomposition reaction of H_2O_2 (Fig. 5b) however probably dominates at higher Au concentration leading to a maximum in H_2O_2 yield with Au content.

Results showing the influence of Pt concentration in the oxidized Pd-Pt/ZrO₂ catalyst on its performance in the H₂ to H_2O_2 oxidation in an aqueous acidic (0.03 H_3PO_4) reaction medium are presented in Fig. 6a. The H₂ conversion activity of the catalyst increased with the increase in the Pt concentration in the catalyst. Similar to the Au case, the H₂O₂ yield also passed through a maximum as a function of Pt content. However, in case of Pt addition, the initial increase in H₂O₂ yield was lower than that observed on Au addition; H2O2 yield increased only by a factor of ~ 1.5 in the Pt case. Interestingly the H_2O_2 yield at higher Pt concentrations quickly dropped below that of monometallic Pd-based catalyst; this was in contrast to the Au case (Fig. 5a). The observed decrease in the H_2O_2 yield/selectivity in the H_2 to H_2O_2 oxidation with the increase in the Pt concentration in the catalyst may be attributed to the increased H₂O₂ decomposition activity of the catalyst (Fig. 6b) and decreasing stability of the hydroperoxy species (precursor for H_2O_2 formation [10,16]) eventually leading to water formation. The decreased stability of the hydroperoxy species at higher Pt content is probably related to the superior ability of Pt to catalyze the scission of the O–O bond [10].

Presence of Ru and Rh in the catalyst was found to be detrimental to the H_2O_2 yields (Figs. 7 and 8). It is apparent that in case of Ru and Rh, the increase in H_2 conversion was not sufficient to compensate for the loss in H_2O_2 selectivity due to increase in the secondary H_2O_2 decomposition (Figs. 7b and 8b) and enhancement of the direct non-selective parallel H_2 to water oxidation side reaction.

4. Concluding remarks

- 1. The H_2 conversion activity of the reduced Pd catalysts was higher than that for the oxidized forms. However, the oxidized Pd catalysts had a significantly higher selectivity for the H_2O_2 formation.
- The H₂O₂ decomposition activity was an order of magnitude higher for the reduced Pd catalysts. Correspondingly the oxidized catalysts showed significantly superior H₂O₂ yields.
- 3. Catalyst properties such as particle size and surface area were found to be less important than the oxidation state in determining the H_2O_2 selectivity.
- 4. The H_2O_2 yield in the H_2 to H_2O_2 oxidation passed through a maximum with increase in the Au concentration. A similar effect was also observed in case of Pt. However, Au was found to be a superior promoter for the direct H_2O_2 synthesis process.
- 5. Presence of Rh and Ru was found to be detrimental for the direct H₂O₂ synthesis process.

Acknowledgments

Chanchal Samanta and V.R. Choudhary are grateful to the CSIR (New Delhi) for the award of a Senior Research Fellowship and the Emeritus Scientist Scheme, respectively.

References

- [1] A. Wood, Chem. Week 166 (2004) 27.
- [2] V.R. Choudhary, A.G. Gaikwad, S.D. Sansare, Angew. Chem. Int. Ed. 40 (2001) 1776.
- [3] V.V. Krishan, A.G. Dokoutchaev, M.E. Thompson, J. Catal. 196 (2000) 117.
- [4] P. Landon, P.J. Papworth, C.J. Kiely, G.J. Hutchings, Chem. Commun. (2002) 2058.
- [5] V.R. Choudhary, A.G. Gaikwad, S.D. Sansare, Catal. Lett. 83 (2002) 235.
- [6] V.R. Choudhary, S.D. Sansare, A.G. Gaikwad, Catal. Lett. 84 (2002) 81.
- [7] A.G. Gaikwad, S.D. Sansare, V.R. Choudhary, J. Mol. Catal. A 181 (2002) 143–173.
- [8] P. Landon, P.J. Collier, A.F. Carley, D. Chadwick, A. Burrows, A.J. Papworth, C.J. Kiely, G.J. Hutchings, Phys. Chem. Chem. Phys. 5 (2003) 1917.
- [9] R. Burch, P.R. Ellis, Appl. Catal. B 42 (2003) 103.
- [10] J.H. Lunsford, J. Catal. 216 (2003) 455.
- [11] G.B. Brieva, E.C. Serrano, J.M.C. Martin, J.L.G. Fierro, Chem. Commun. (2004) 1184.
- [12] S. Chinta, J.H. Lunsford, J. Catal. 225 (2004) 249.
- [13] V.R. Choudhary, C. Samanta, A.G. Gaikwad, Chem. Commun. (2004) 2054.
- [14] V.R. Choudhary, A.G. Gaikwad, React. Kinet. Catal. Lett. 80 (2003) 27.
- [15] V.R. Choudhary, M.G. Parande, P.H. Brahame, Ind. Eng. Chem. Fundam. 21 (1982) 472.
- [16] S. Chinta, T.V. Choudhary, L.L. Daemen, J. Eckert, D.W. Goodman, JACS 126 (2004) 38.